

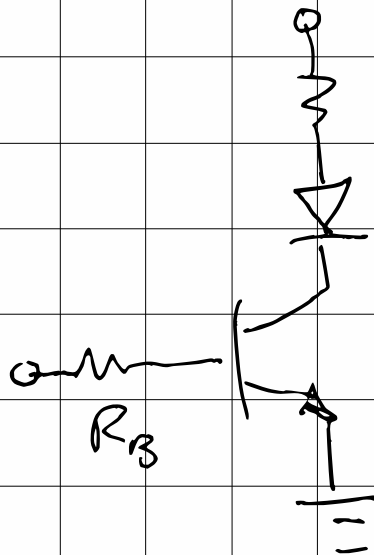
ME 133

Lecture 8

1/27/2022

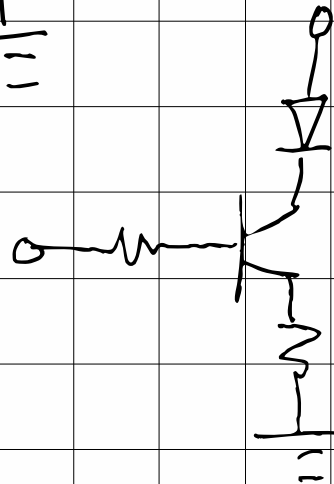
last time :

o

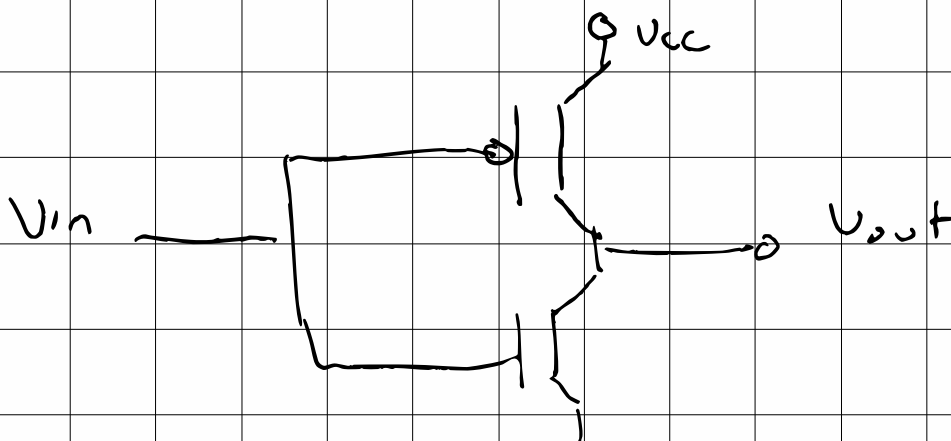


BJT switch

For your lab:



o FET overview



Question last time:

Can you put too much
current at Base of the
BJT switch.

→ ~~Short~~ Short answer, probably not.

→ main considerations:

① power consumption

② Time to switch off
depends I_B

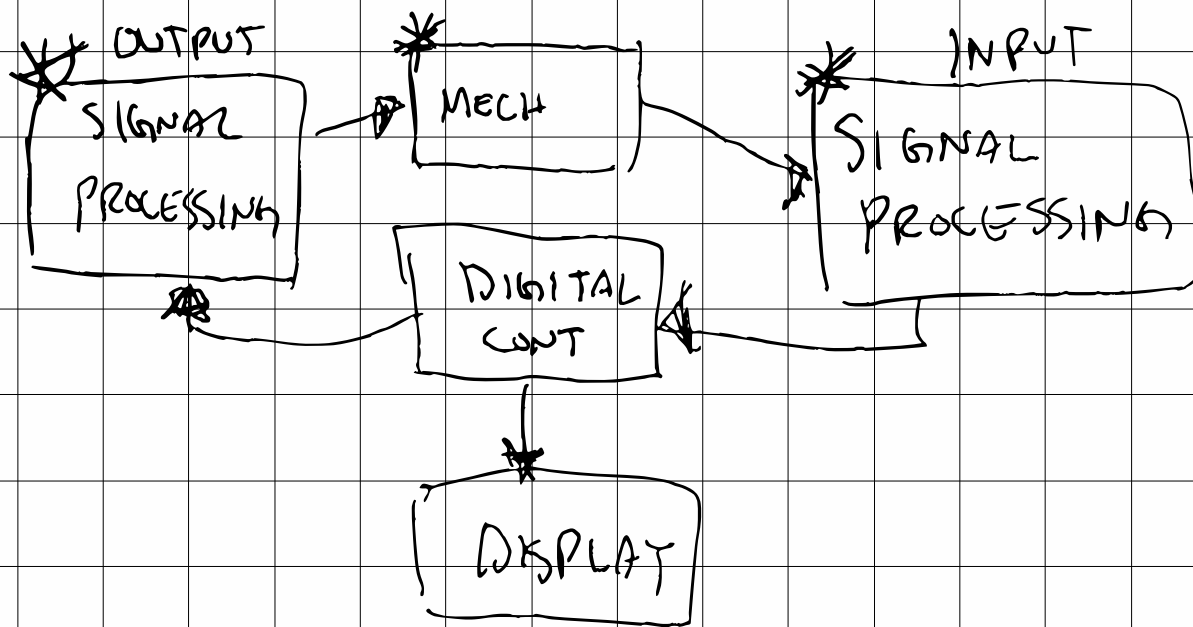
Today:

Chapter 4/

(1) Amplitude Linearity

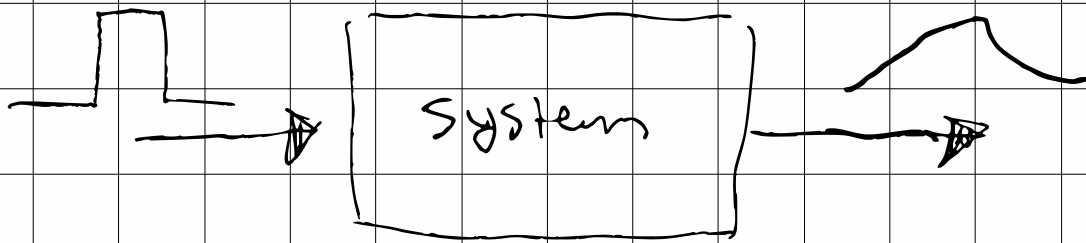
(2) Bandwidth

Ch. 1: System Response



Goal: mathematically model physical systems
& characterize the response to
dynamic inputs.

Response : given an input
what does the output look
like



We will consider "measurement system" for
our discussion, but theory applies to
any system.

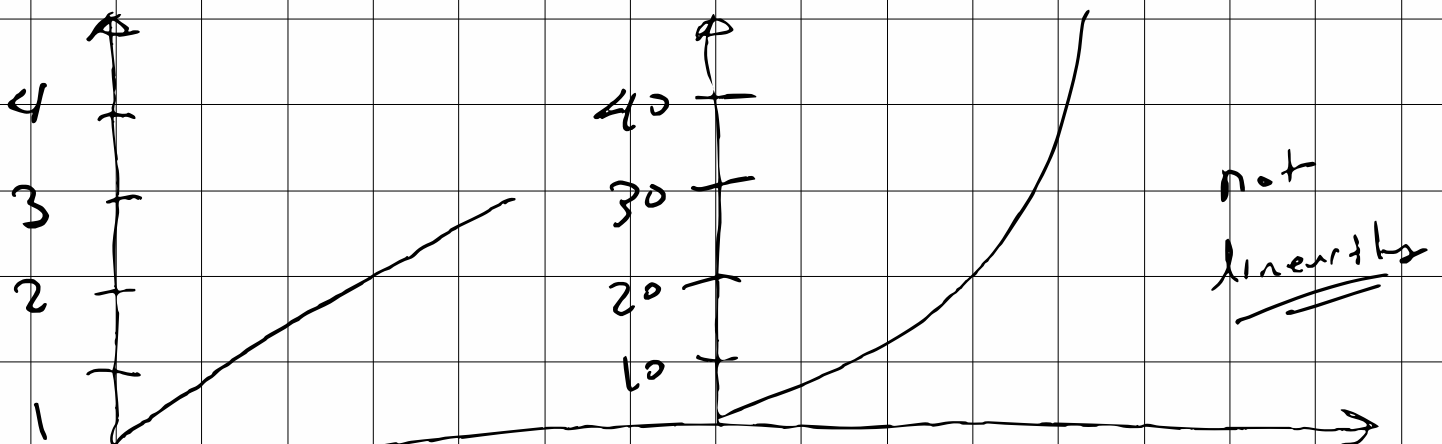
What make a good measurement system?

- ① Amplitude linearity
 - ② Adequate Bandwidth
 - ③ Phase linearity
- } today

Amplitude linearity

$$V_{out}(t) - V_{out}(0) = \alpha \left[V_{in}(t) - V_{in}(0) \right]$$

Constant of proportionality



Fourier Analysis (steady state)

Main Idea: Any periodic signal can be represented as an infinite sum of sine & cosine waveforms of different amplitude & freq.

Fundamental Harmonic: $\omega_0 = \frac{2\pi}{T} = 2\pi f_0$

$\underbrace{\quad}_{\text{rad/s}} \qquad \uparrow \text{period} \qquad \underbrace{\quad}_{\text{Hz}}$

→ all other frequencies in the Fourier representation are integer multiples of ω_0

Fourier series Representation

$$F(t) = C_0 + \sum_{n=1}^{\infty} A_n \cos(n\omega_0 t) + \sum_{n=1}^{\infty} B_n \sin(n\omega_0 t)$$

DC
component

$$A_n = \frac{2}{T} \int_0^T f(t) \cos(n\omega_0 t) dt$$

$$B_n = \frac{2}{T} \int_0^T f(t) \sin(n\omega_0 t) dt$$

$$C_0 = \frac{1}{T} \int_0^T f(t) dt = \frac{A_0}{2}$$

$$F(t) = C_0 + \sum_{n=1}^{\infty} C_n \cos(n\omega_0 t + \phi_n)$$

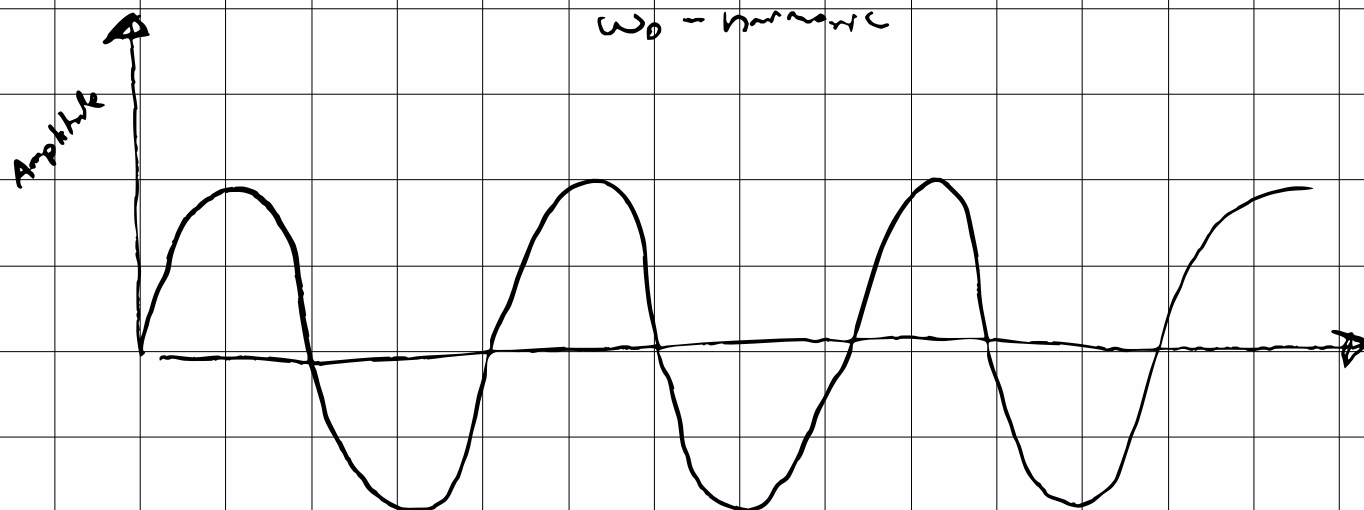
$$C_n = \sqrt{A_n^2 + B_n^2}$$

$$\phi_n = -\tan^{-1}\left(\frac{B_n}{A_n}\right)$$

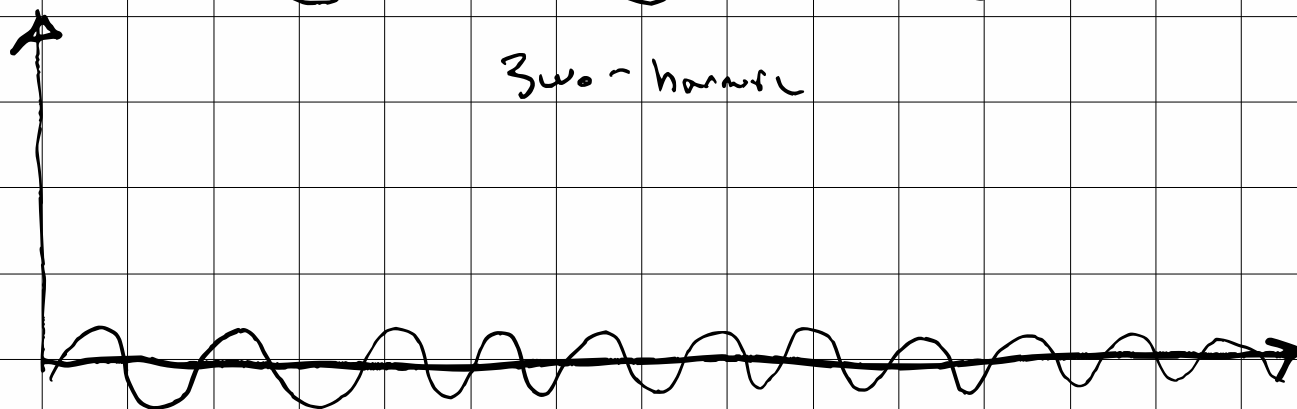
Single amplitude version.



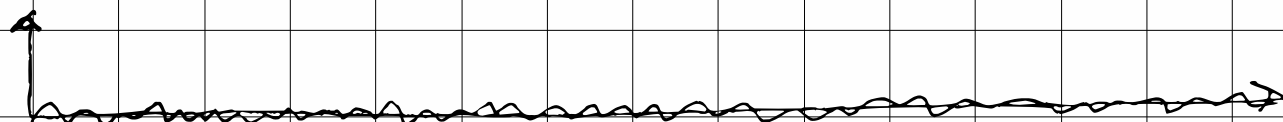
ω_0 - harmonic

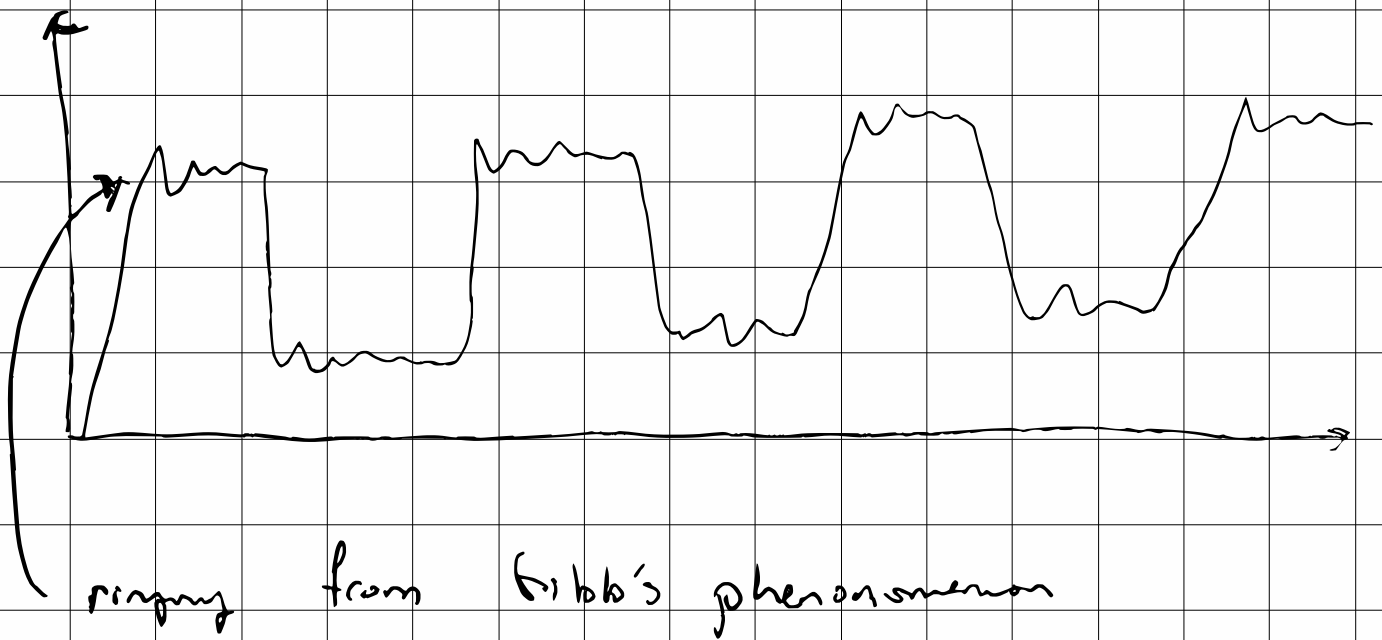


$3\omega_0$ - harmonic

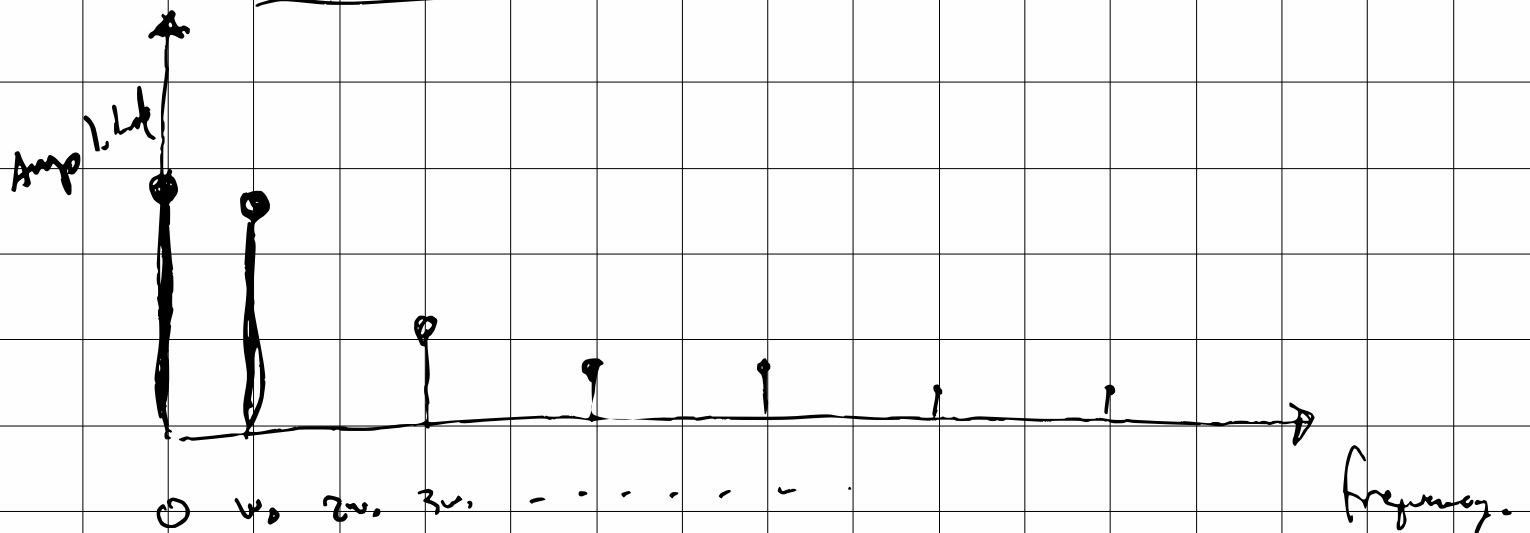


$5\omega_0$ - harmonic





Spectrum of $\text{Sqr}(t)$



* must use single-amplitude version of Fourier Series.

Bandwidth & Frequency Response

- Ideally a measurement system should replicate all frequency components of the input.

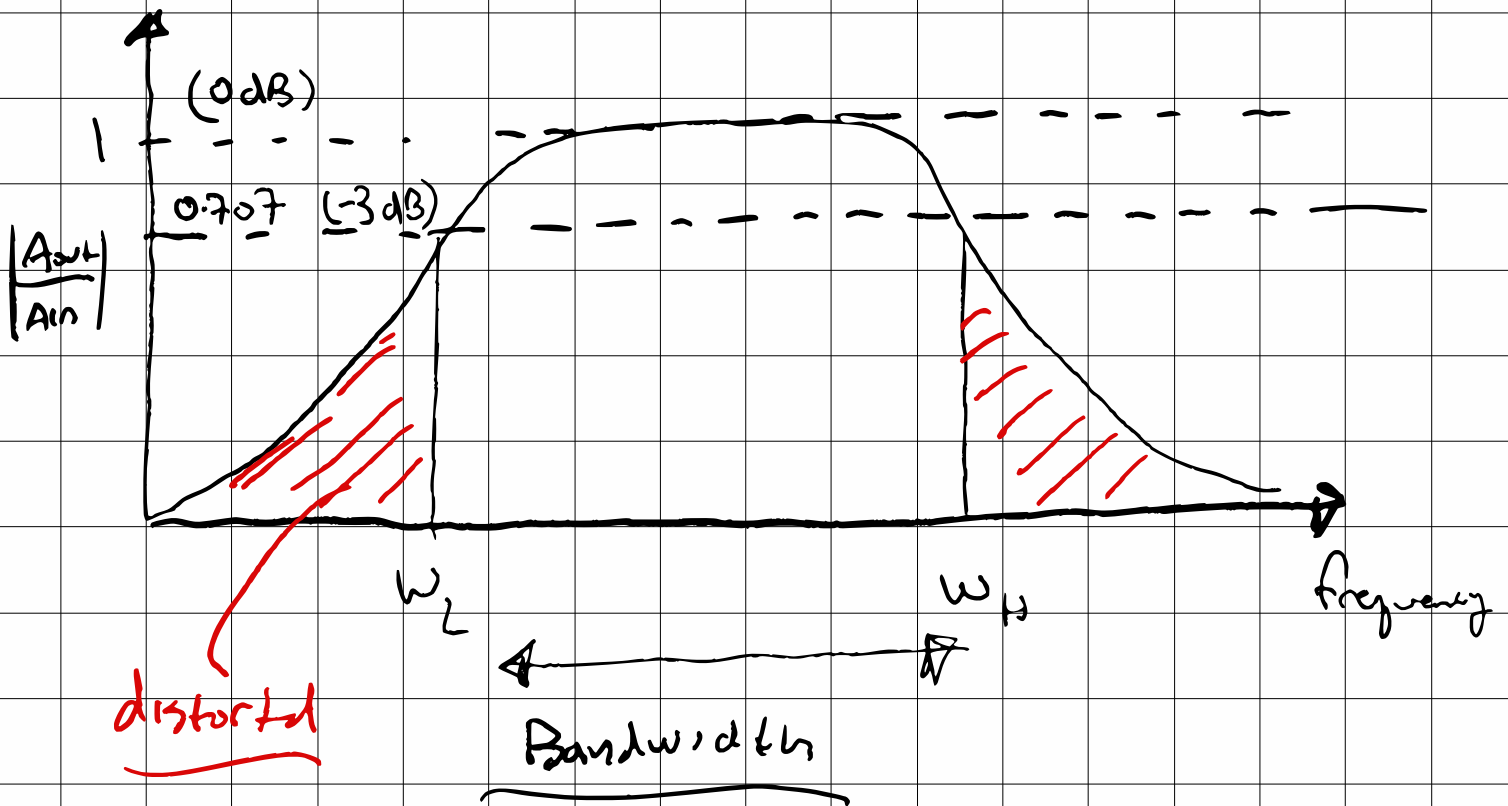
→ Decibels:

$$\text{dB} = 20 \log_{10} \left(\frac{A_{\text{out}}}{A_{\text{in}}} \right)$$

(computed at each frequency!)

0	dB	→	$A_{\text{out}} = A_{\text{in}}$
20	dB	→	$A_{\text{out}} = 10 \cdot A_{\text{in}}$
40	dB	→	$A_{\text{out}} = 100 \cdot A_{\text{in}}$
60	dB	→	$A_{\text{out}} = 1000 \cdot A_{\text{in}}$

Frequency Response Curve



Bode Plot

Bandwidth is the range $\omega_L \rightarrow \omega_H$

• Why -3 dB ?

"half-power points"

$$\frac{P_{\text{out}}}{P_{\text{in}}} = \frac{1}{2}$$

$$\rightarrow P = V^2 \cdot R$$

$$\therefore P \sim V^2$$

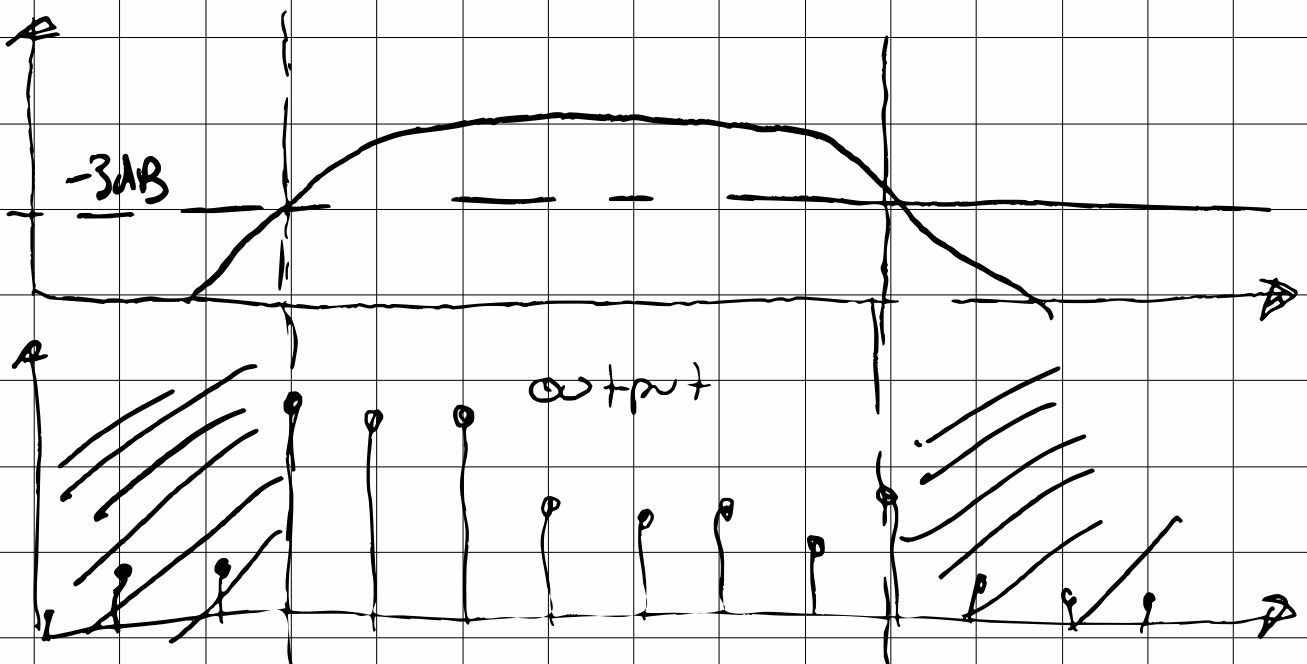
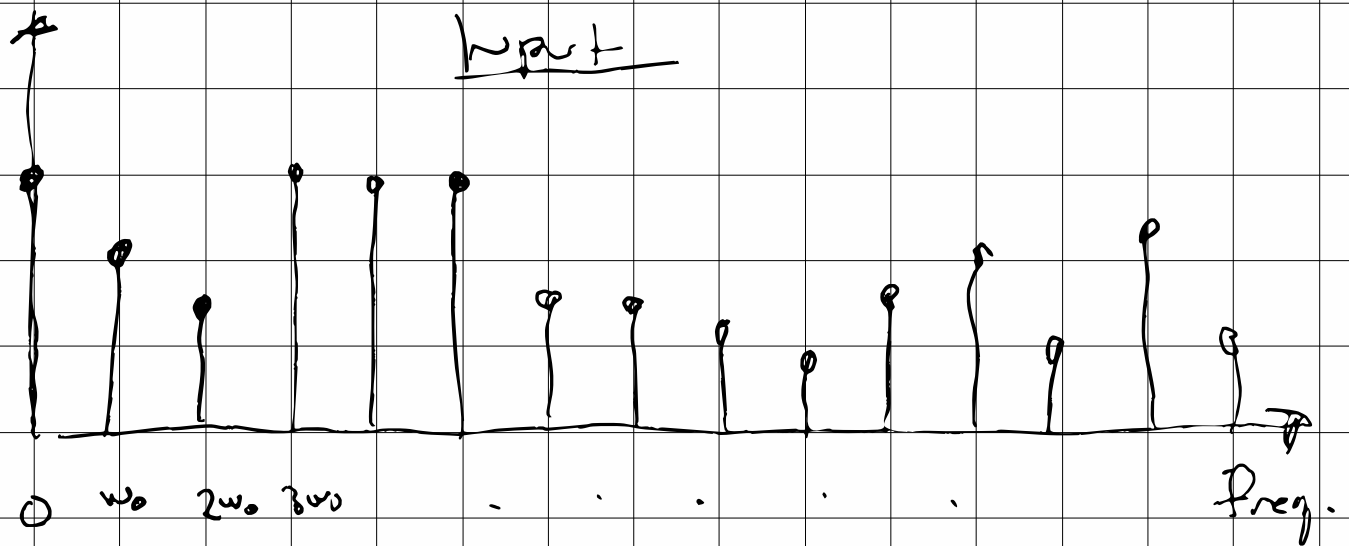
$$\frac{A_{\text{out}}}{A_{\text{in}}} = \sqrt{\frac{P_{\text{out}}}{P_{\text{in}}}} = \frac{1}{\sqrt{2}} \approx 0.707$$

$$\text{dB} = 20 \log_{10} \left(\frac{1}{\sqrt{2}} \right) \approx \underline{\underline{-3 \text{ dB}}}$$

$\omega_c \rightarrow \omega_{ct}$ $\rightarrow$ cutoff freq.
or corner freq.

large bandwidth $\rightarrow$ high fidelity

If you know the frequency response of your system (measurement device, sensor, actuator, filter) and you know the freq. content of the input, then you can predict the out freq. content.



- How to determine bandwidth of a system?

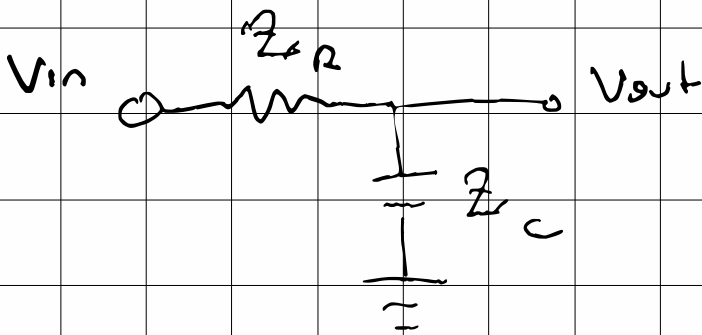
→ Field "System Identification"

→ send pure sine waves as input for all frequency.

→ frequency sweep!

→ Gaussian noise

Example: lowpass filter.



$$V_{out} = \left(\frac{Z_R}{Z_R + Z_C} \right) V_{in}$$

$$Z_C = \frac{1}{j\omega C} \quad \Rightarrow \quad \frac{V_{out}}{V_{in}} = \frac{1}{j\omega RC + 1}$$

$$Z_R = R$$

$$\frac{V_{out}}{V_{in}} = \frac{1}{j\omega RC + 1}$$

$$\left| \frac{V_{out}}{V_{in}} \right| = \frac{1}{\sqrt{1 + (\omega RC)^2}}$$

$$\text{let } \omega_c = \frac{1}{RC}$$

$$\left| \frac{V_{out}}{V_{in}} \right| = \frac{1}{\sqrt{1 + (\omega/\omega_c)^2}}$$

↖ next time

