

1. The forward kinematics for the articulate robot shown in Fig. 2 can be described from the following individual transformation matrices:

$$\begin{aligned}
 {}^0T_1 &= \begin{bmatrix} c\theta_1 & 0 & s\theta_1 & 0 \\ s\theta_1 & 0 & -c\theta_1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} &
 {}^1T_2 &= \begin{bmatrix} s\theta_2 & -s\theta_1 & 0 & l_2c\theta_2 \\ c\theta_2 & c\theta_1 & 0 & l_2s\theta_2 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} &
 {}^2T_3 &= \begin{bmatrix} c\theta_3 & 0 & s\theta_3 & 0 \\ s\theta_3 & 0 & -c\theta_3 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
 {}^3T_4 &= \begin{bmatrix} c\theta_4 & 0 & s\theta_4 & 0 \\ s\theta_4 & 0 & -c\theta_4 & 0 \\ 0 & -1 & 0 & l_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} &
 {}^4T_5 &= \begin{bmatrix} c\theta_5 & 0 & s\theta_5 & 0 \\ s\theta_5 & 0 & -c\theta_5 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} &
 {}^5T_6 &= \begin{bmatrix} c\theta_6 & -s\theta_6 & 0 & 0 \\ s\theta_6 & c\theta_6 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}
 \end{aligned}$$

Find the 6×6 Jacobian matrix using *Jacobian generating vectors*:

$$J(\mathbf{q}) = [\mathbf{c}_1(\mathbf{q}) \quad \mathbf{c}_2(\mathbf{q}) \quad \cdots \quad \mathbf{c}_6(\mathbf{q})].$$

2. Consider the geometric Jacobian:

$$J(\mathbf{q}) = \begin{bmatrix} J_D \\ J_R \end{bmatrix} = \begin{bmatrix} -s\theta_1s\theta_2d_3 - c\theta_1l_2 & c\theta_1c\theta_2d_3 & c\theta_1s\theta_2 \\ c\theta_1s\theta_2d_3 - s\theta_1l_2 & s\theta_1c\theta_2d_3 & s\theta_1s\theta_2 \\ 0 & -s_2d_3 & c\theta_2 \\ 0 & -s_1 & 0 \\ 0 & c_1 & 0 \\ 1 & 0 & 0 \end{bmatrix}, \quad \mathbf{q} = \begin{bmatrix} \theta_1 \\ \theta_2 \\ d_3 \end{bmatrix}$$

Find the values of \mathbf{q} that result in singularities in the *displacement* Jacobian, J_D .

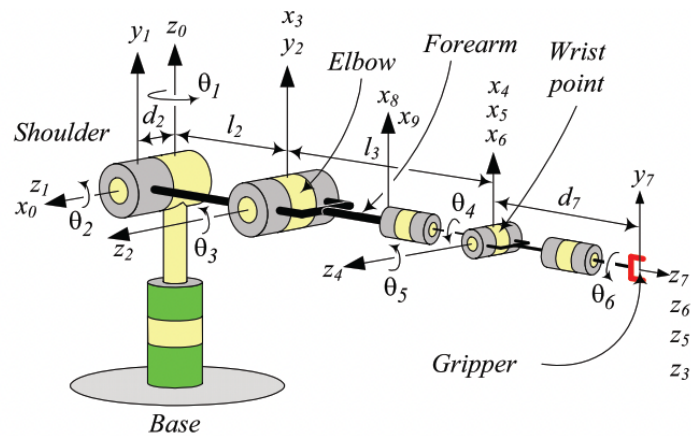


Figure 1: Schematic for Problem 1

3. Suppose you have a dynamic model of a robot in the form:

$$\tilde{M}(\mathbf{q})\ddot{\mathbf{q}} + \tilde{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \tilde{g}(\mathbf{q}) = \boldsymbol{\tau}$$

- Derive an expression for the control variable $\boldsymbol{\tau}$ using the *computed torque controller*.
- Draw a block diagram of the controller and plant (robot), with all relevant signals labeled.

4. Show that the robot dynamics can be expressed in terms of the end-effector variables \mathbf{x} :

$$\Lambda(\mathbf{q})\ddot{\mathbf{x}} + \Gamma(\mathbf{q}, \dot{\mathbf{x}})\dot{\mathbf{x}} + \eta(\mathbf{q}) = \mathbf{F}$$

with

$$\begin{aligned}\Lambda(\mathbf{q}) &= J^{-T}(\mathbf{q})M(\mathbf{q})J^{-1}(\mathbf{q}), \\ \Gamma &= J^{-T}(\mathbf{q})C(\mathbf{q}, \dot{\mathbf{q}})J^{-1}(\mathbf{q}) - \Lambda(\mathbf{q})\dot{J}(\mathbf{q})J^{-1}(\mathbf{q}), \\ \eta(\mathbf{q}) &= J^{-T}(\mathbf{q})g(\mathbf{q})\end{aligned}$$

and \mathbf{F} is the total force (wrench) at the end-effector.

5. Find and plot a polynomial path for a single joint coordinate that satisfies the following conditions:

- $q(1) = 0$, $\dot{q}(1) = 0$, $q(2) = \pi/2$, $q(3) = 0$, $\dot{q}(3) = 0$
- $q(1) = 0$, $\dot{q}(1) = 0$, $q(2) = \pi/2$, $q(2.5) = -\pi/2$, $q(3) = 0$, $\dot{q}(3) = 0$
- $q(1) = 0$, $\dot{q}(1) = 0$, $q(1.5) = \pi/2$, $\dot{q}(1.5) = -\pi/16$, $q(2.5) = -\pi/2$, $\dot{q}(2.5) = \pi/16$, $q(3) = 0$, $\dot{q}(3) = 0$

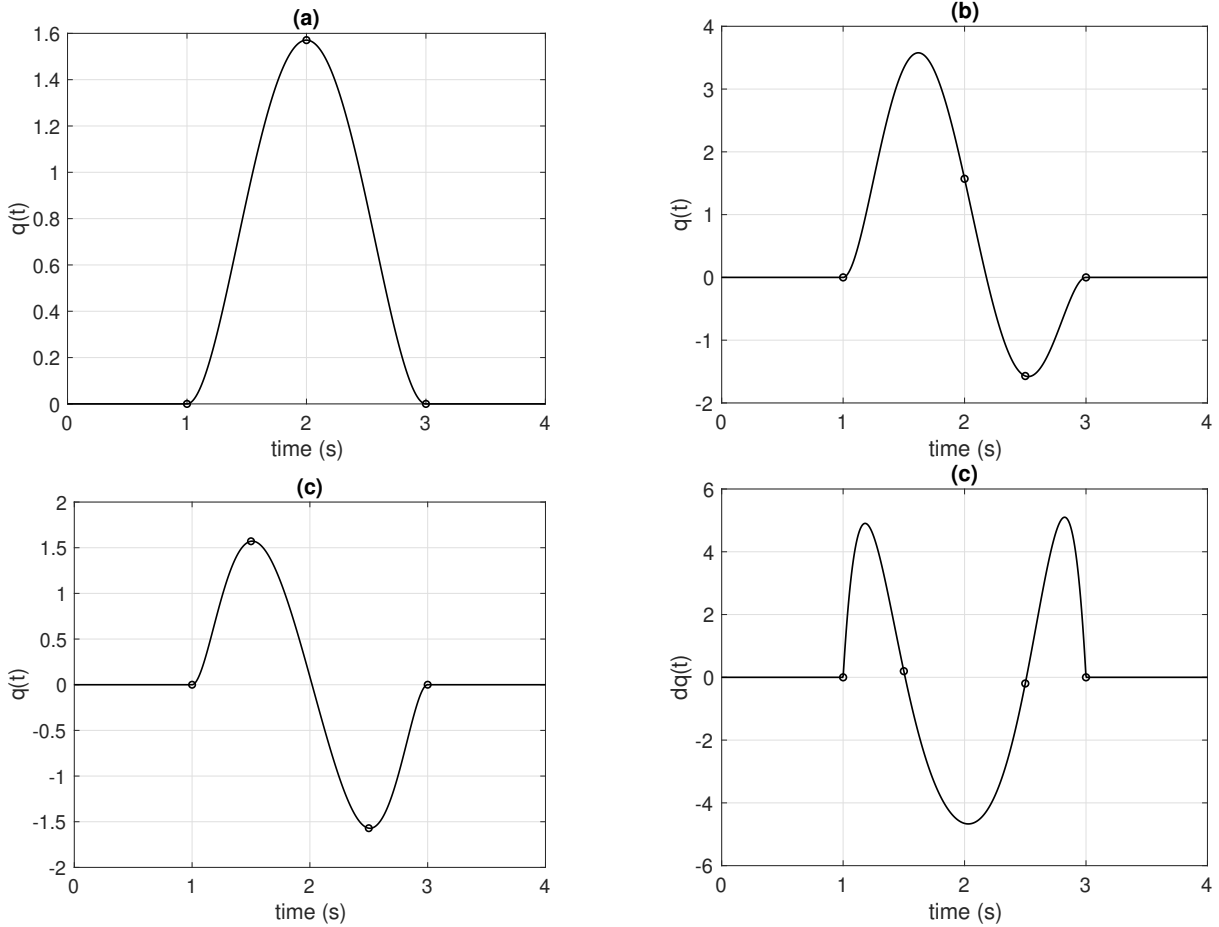


Figure 2: Solution plots for Problem 5