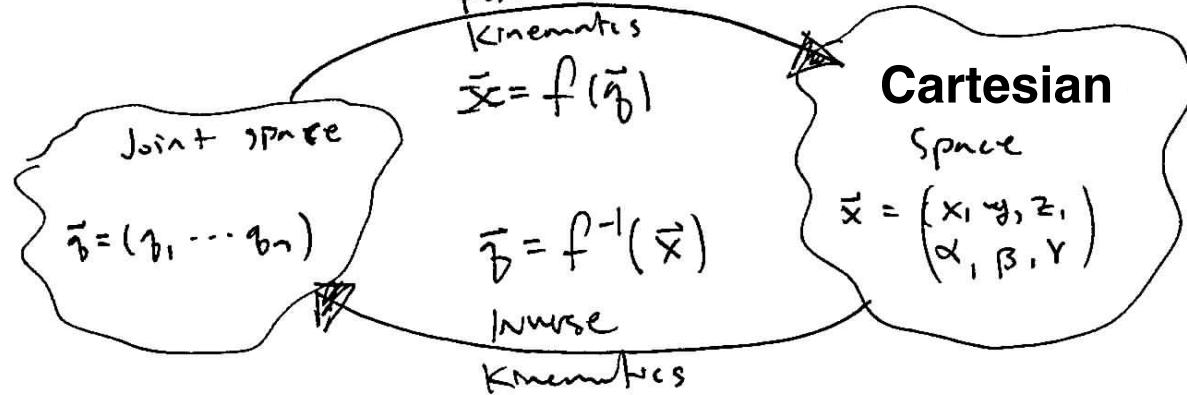


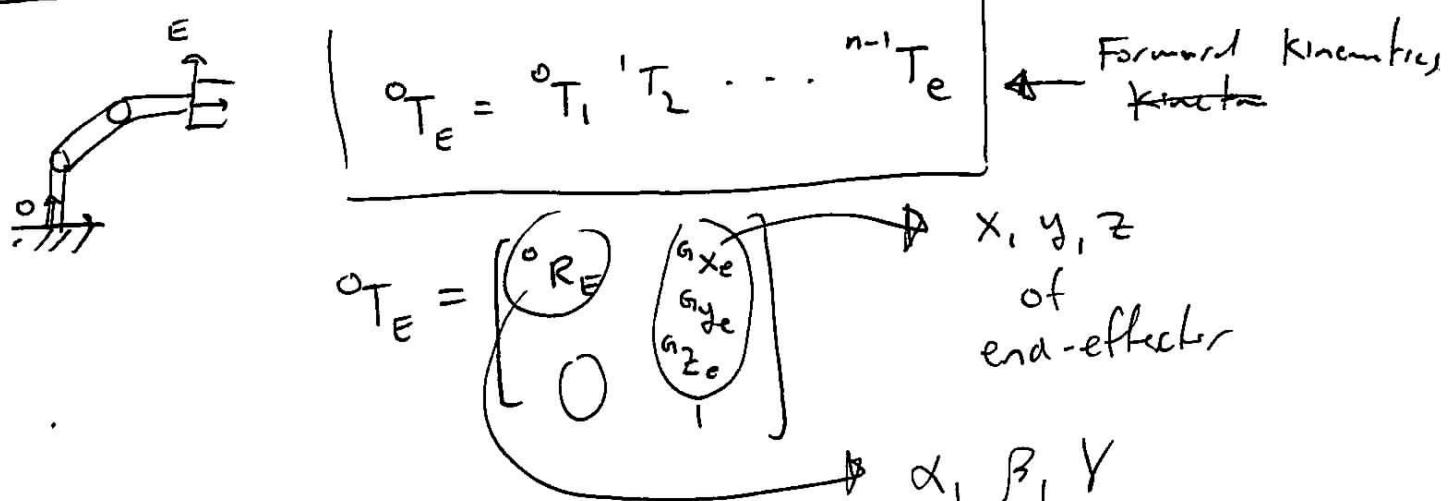
Last time: Forward Kinematics



- use DH-parameters as a systematic approach to assign coordinates frame to joints

$$\begin{aligned} g_i : & \left. \begin{array}{l} a_i : \text{link length} \\ \alpha_i : \text{link twist} \\ d_i : \text{joint distance} \\ \theta_i : \text{joint angle} \end{array} \right\} \\ & \text{completely define coordinate transform } i-1 \rightarrow i \end{aligned}$$

$${}^{i-1}T_i = f(a_i, \alpha_i, d_i, \theta_i)$$



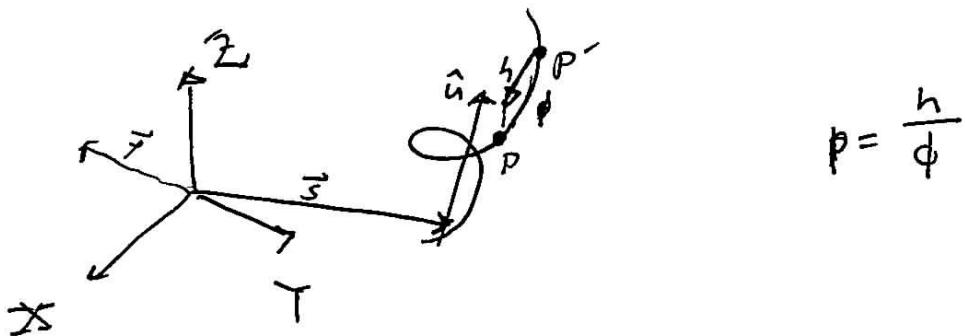
Today:

- screw coordinates
 - Product of Exponentials (PoE)
 - Intro - Inverse Kinematics
-

Screw Coordinates : ~~generalization~~
~~generalized~~ approach
to multi-body mechanics

Basic Idea : (Chasles Theorem)

All displacements can be produced by
a single rotation combined with a
translation along some axis:



$$p = \frac{h}{\phi}$$

$${}^G S_B(h, \phi, \hat{u}, \vec{s}) = \begin{bmatrix} {}^G R_B & {}^G \vec{s} - {}^G R_B {}^G \vec{s} + h \hat{u} \\ 0 & 1 \end{bmatrix}$$

h : translation

ϕ : rotation

\hat{u} : axis

\vec{s} : location vector

Inverse Screw :

$${}^B \tilde{S}^{-1} (h, \phi, \hat{u}, \vec{s}) = {}^B \tilde{S}_h (h, \phi, \hat{u}, \vec{s})$$

$$= \begin{bmatrix} {}^G R_B^T & h \vec{s} - {}^G R_B^T {}^G \vec{s} - h \hat{u} \\ 0 & 1 \end{bmatrix}$$

$$T = \tilde{S}(h, \phi, \hat{u}, \vec{s}) = \begin{bmatrix} e^{\phi \tilde{u}} & (I - e^{\phi \tilde{u}}) \vec{s} + h \hat{u} \\ 0 & 1 \end{bmatrix}$$

\tilde{u} : skew symmetric version of \hat{u}

Q: Can we write entire transformation as a matrix exponential? Yes!

Screw Axis

$$\begin{bmatrix} \tilde{u} \\ \vec{r} + p \hat{u} \end{bmatrix} \xrightarrow{\text{displacement}} \begin{bmatrix} \hat{u} \\ \vec{r} + p \hat{u} \end{bmatrix} \quad \begin{array}{l} \text{Plücker} \\ \text{Coordinate} \end{array}$$

$\frac{4 \times 1}{\text{Screw axis}}$

$$\begin{bmatrix} \vec{f} = -\hat{u} \times \vec{s} \\ p = \frac{h}{\phi} \end{bmatrix}$$

$$\begin{bmatrix} \tilde{u} & \vec{r} + p \hat{u} \\ 0 & 0 \end{bmatrix} \phi$$

$$T = e^{\tilde{S} \phi}$$

③

$$\tilde{S} = \begin{bmatrix} \hat{u} \\ \vec{\varphi} + p\hat{u} \end{bmatrix} \quad \text{Plücker coordinate (Screw Axis)}$$

$$T_p = e^{\tilde{S}\phi} \quad T_p^{(0)} \xrightarrow{\uparrow} \begin{bmatrix} x_p \\ y_p \\ z_p \\ 1 \end{bmatrix}$$

$$\tilde{S} = \begin{bmatrix} \hat{u} & \vec{\varphi} + p\hat{u} \\ 0 & 0 \end{bmatrix}$$

1×4

$P = \infty$ pure translation

$$\tilde{S} = \begin{bmatrix} 0 \\ \hat{u} \end{bmatrix} \quad \underline{\text{Prismatic joint}}$$

$P = 0$ pure rotation

$$\tilde{S} = \begin{bmatrix} \hat{u} \\ \vec{\varphi} \end{bmatrix} \quad \vec{\varphi} = -\hat{u} \times \vec{s} \quad \underline{\text{Revolute joint}}$$

Product of Exponentials For Forward Kinematics

- base frame is End effector
 - Homogeneous Transformation M ($\gamma = 0$)

Murray ch.3-2
Lynch ch. 4

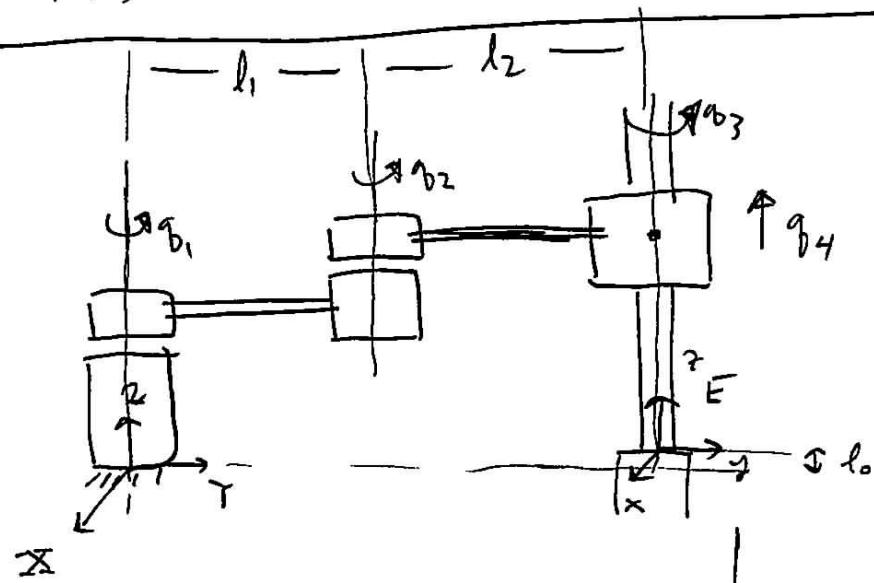
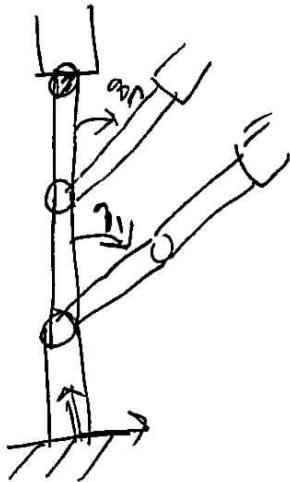
- define axis of motion

- Find screw axis \tilde{S} for each joint

~~- POF~~ \bullet $O_T = e^{\tilde{S}_1 \phi_1} e^{\tilde{S}_2 \phi_2} \dots e^{\tilde{S}_n \phi_n} M$

• POE:

$${}^0T_E = e^{\tilde{s}_1 \tilde{q}_1} \cdots e^{\tilde{s}_m \tilde{q}_m} e^{\tilde{s}_M M}$$



$$M = \begin{bmatrix} I & \begin{bmatrix} 0 \\ l_1 + l_2 \\ l_0 \end{bmatrix} \\ 0 & 1 \end{bmatrix}$$

$$\tilde{s} = \begin{bmatrix} 0 \\ \hat{u} \end{bmatrix} \quad \text{prismatic joint}$$

$$\tilde{s} = \begin{bmatrix} \hat{u} \\ \vec{\tau} \end{bmatrix} \quad \text{revolute} \quad \vec{\tau} = -\hat{u} \times \vec{s}$$

$$\begin{aligned} \hat{u}_1 &= \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} & \tilde{s}_1 &= \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \end{bmatrix} \\ \vec{s}_1 &= \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \end{aligned}$$

$$\hat{u}_2 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} / -\begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \times \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} l_1 \\ 0 \\ 0 \end{bmatrix}$$

$$\begin{aligned} \vec{s}_1 &= \begin{bmatrix} 0 \\ l_1 \\ 0 \end{bmatrix} & \tilde{s}_2 &= \begin{bmatrix} 0 \\ 0 \\ 1 \\ l_1 \\ 0 \\ 0 \end{bmatrix} \end{aligned}$$

$$\begin{array}{l}
 \vec{s}_3 = ? \\
 \hat{\vec{u}}_3 = ? \\
 \vec{s} = ?
 \end{array}
 \Rightarrow \left[\begin{array}{c} \hat{\vec{u}}_3 \\ -\hat{\vec{u}}_3 \times \vec{s}_3 \end{array} \right] \quad \left| \begin{array}{l}
 \hat{\vec{u}}_3 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\
 \vec{s} = \begin{bmatrix} 0 \\ l_1 + l_2 \\ 0 \end{bmatrix} \\
 -\hat{\vec{u}}_3 \times \vec{s} = \begin{bmatrix} l_1 + l_2 \\ 0 \\ 0 \end{bmatrix}
 \end{array} \right. \quad \vec{s}_3 = \begin{bmatrix} 0 \\ 0 \\ l_1 + l_2 \end{bmatrix}$$

$$\begin{array}{l}
 \hat{\vec{u}}_1 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\
 \vec{s}_1 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} \\
 \vec{s} = 0
 \end{array}$$

$${}^0 T_4 = e^{\tilde{s}_1 \tilde{b}_1} e^{\tilde{s}_2 \tilde{b}_2} e^{\tilde{s}_3 \tilde{b}_3} e^{\tilde{s}_4 \tilde{b}_4} M$$

Some advantages

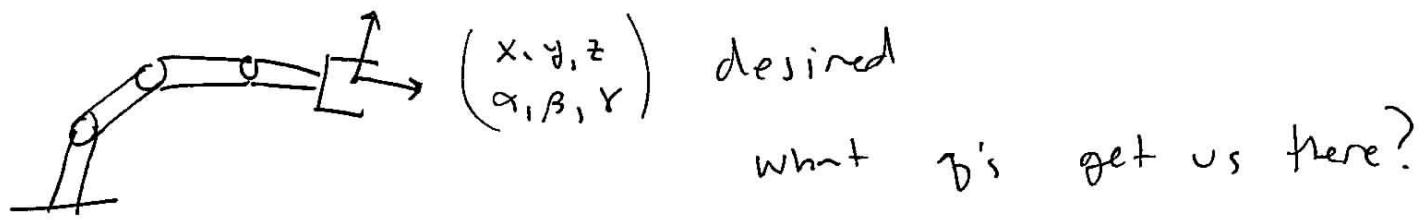
- ignore the in-between transformation
- finds velocity -

Some disadvantages

- ${}^{i-1} T_i$ not given explicitly

POE

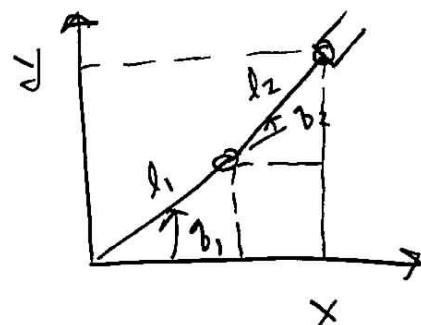
Inverse Kinematics



$${}^0T_e, \text{desired} = \begin{bmatrix} {}^0R_e & {}^0x_e \\ 0 & {}^0y_e \\ 0 & {}^0z_e \\ 0 & 1 \end{bmatrix}$$

$${}^0T_e(\vec{q}) = {}^0T_e, \text{desired}$$

Planar RR robot IK



$$\vec{x} = \begin{bmatrix} x \\ y \end{bmatrix}$$

$$\vec{q} = \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$

$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2) \\ l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2) \end{bmatrix}$$

$$\begin{array}{l}
 x^2 = (\ell_1 c_1 + \ell_2 c_{12})^2 \\
 = \ell_1^2 c_1^2 + 2\ell_1 \ell_2 c_1 c_{12} + \ell_2^2 c_{12}^2 \\
 y^2 = \ell_1^2 s_1^2 + 2\ell_1 \ell_2 s_1 s_{12} + \ell_2^2 s_{12}^2
 \end{array}$$

$$\begin{aligned}
 x^2 + y^2 &= \cancel{\ell_1^2 + \ell_2^2} \\
 x^2 + y^2 &= \ell_1^2 (c_1^2 + \cancel{s_1^2}) + \ell_2^2 (\cancel{\ell_{12}^2} + \cancel{s_{12}^2}) \\
 &\quad + 2\ell_1 \ell_2 [c_1 c_{12} + \cancel{s_1 s_{12}}] \\
 &= \underline{\ell_1^2 + \ell_2^2} + \underline{(2\ell_1 \ell_2 [c_1 c_{12} + s_1 s_{12}])}
 \end{aligned}$$

$$c_{12} = \cos(\beta_1 + \beta_2) = \cos \beta_1 \cos \beta_2 - \sin \beta_1 \sin \beta_2$$

$$s_{12} = \sin(\beta_1 + \beta_2) = \sin \beta_1 \cos \beta_2 + \cos \beta_1 \sin \beta_2$$

$$\Rightarrow 2\ell_1 \ell_2 [c_1 c_{12} + s_1 s_{12}] = 2\ell_1 \ell_2 [c_1(c_1 c_2 - s_1 s_2) + s_1(s_1 c_2 + c_1 s_2)]$$

$$2\ell_1 \ell_2 [c_2] = 2\ell_1 \ell_2 \cos \beta_2$$

$$x^2 + y^2 = \ell_1^2 + \ell_2^2 + 2\ell_1 \ell_2 \cos \beta_2$$

$$\cos \beta_2 = \frac{(x^2 + y^2) - (\ell_1^2 + \ell_2^2)}{2\ell_1 \ell_2}$$